

Enhanced Transport in Ammonia Slip Catalyst (ASC) Washcoat by using Sacrificial Agents

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Highlights

- ASC: Noted increase in NH₃ conversion while maintaining N₂ selectivity
- SCR: Adequate improvement in NO/NH₃ conversion
- Monolith reactor model predicts and optimizes enhancement

1. Introduction

A dual-layer Ammonia Slip Catalyst (ASC) with base precious group metal (PGM) and top selective catalytic reduction of NO_x by NH₃ (NH₃-SCR) layer is commonly used for selective oxidation of NH₃ to N₂. The top SCR (e.g. Cu/Chabazite) layer increases N₂ selectivity at the expense of NH₃ conversion by restricting diffusion of reacting species. To enhance gas transport, the sacrificial agents (including yeast and poly-tert-butyl-acrylate) are used to create calcined holes in SCR layer, increasing the porosity [1]. While keeping a fixed catalyst loading, the dual-layer ASC with modified top SCR layer exhibits a significant increase in NH₃ conversion without affecting the desired product N₂ selectivity. Similar improvements in the NO/NH₃ conversion are achieved with a standalone SCR layer for the standard NH₃+NO reaction.

2. Methods

Catalyst slurry preparation: For the PGM layer, Pt/Al₂O₃ catalyst powder was synthesized using wetness impregnation with Pt precursor hexahydrate chloroplatinic acid. An estimated amount of precursor was added to achieve the target loading of Pt(1.5 g/ft³) and the corresponding Pt/Al₂O₃ washcoat loading of 1.5 g/in³. The Pt/Al₂O₃ slurry was prepared by mixing Pt/Al₂O₃, water and boehmite (20 wt% AlOOH) in mass ratio of 4:8:5. For the SCR layer, the powdered catalyst Cu/SSZ-13 used in the experiments was provided by Johnson Matthey Inc. Three different slurries of Cu/SSZ-13 were prepared by mixing powdered Cu/SSZ-13, water and boehmite (20 wt% AlOOH) in mass ratio of 4:8:5. The slurries were then ball milled for 20 h. Out of three Cu/SSZ-13 slurries prepared, one was kept as it is, while active dry yeast was added to second and polymer (poly-tert-butyl acrylate) was added to third slurry.

Monolith coating: For the dual-layer ASC, the base Pt/Al₂O₃ layer was deposited by dipping blank monoliths in Pt/Al₂O₃ slurry, followed by drying at 120 °C and calcining at 500 °C. For the unmodified dual-layer ASC, the monolith already coated with Pt/Al₂O₃ layer was dipped in Cu/SSZ-13 slurry for 30 s and excess slurry removed by blowing air for 10 s followed by drying in oven at 120 °C for 2 h. For the modified dual-layer ASC, the Cu/SSZ-13 slurry with yeast was used to prepare the top layer. Similarly, Cu/SSZ-13 slurry containing polymer was used for making the other modified type of dual-layer samples. The modified dual-layer samples were dried at room temperature for 2 h. The dipping and drying procedure was repeated to achieve required loading. Once the expected loading was met, the normal dual-layer sample was calcined at 500 °C for 5 h using temperature ramp up/down of 0.5 °C/min. The modified dual-layer samples containing yeast or polymer in the top layer were calcined in flow reactor at 500 °C for 2 h using temperature ramp up rate of 3 °C/min.

For SCR monolith, the blank monoliths were coated with Cu-SSZ-13 following above procedure.

Samples: aPt(b)Cu(c)y – [here, a is monolith sample length, b is Pt loading in g/ft³, c is Cu-SSZ-13 loading in g/in³, y and p for yeast and polymer, no index for conventional dual-layer]

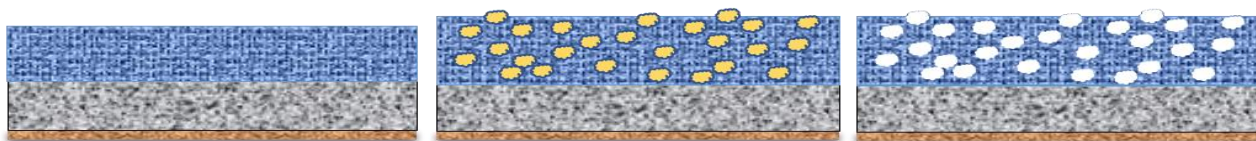


Figure 1. [Left] - Conventional dual-layer ASC (base Pt/Al₂O₃ and top Cu-SSZ-13), [Middle] – Modified dual-layer with yeast/polymer in top layer, [Right] – Modified dual-layer after calcination at 500 °C.

3. Results and discussion

The modified dual-layer ASC outperformed conventional dual-layer in NH₃ conversion (Fig. 2, left) for NH₃ oxidation reaction and negligibly affected N₂ selectivity (results not shown for brevity) [2]. The results showed that the more porous and thicker SCR washcoat layer has better transport properties than the thinner and less porous SCR layer. A dual-layer monolith reactor model predicted the noted decline in the ratio τ/ε (tortuosity/porosity) of the modified washcoat. In another experiment, the NH₃ conversion using the modified dual-layer with Pt(1.5) is comparable to the conventional dual-layer with Pt(4.5) at the same GHSV of 332k h⁻¹. The use of the sacrificial agent could reduce the PGM requirements by up to 60%.

Similarly, the SCR reaction results (Fig. 2, right) showed noticeable improvement in temperature regime (250 °C – 400 °C) by using a modified single layer SCR. At temperatures above 250 °C, the NO conversion of the modified sample with 2.1 g/in³ loading is comparable to conventional SCR sample with 3.2 g/in³ loading. Improvement in gas transport through washcoat can cut the amount of Cu-SSZ-13 by ~30%.

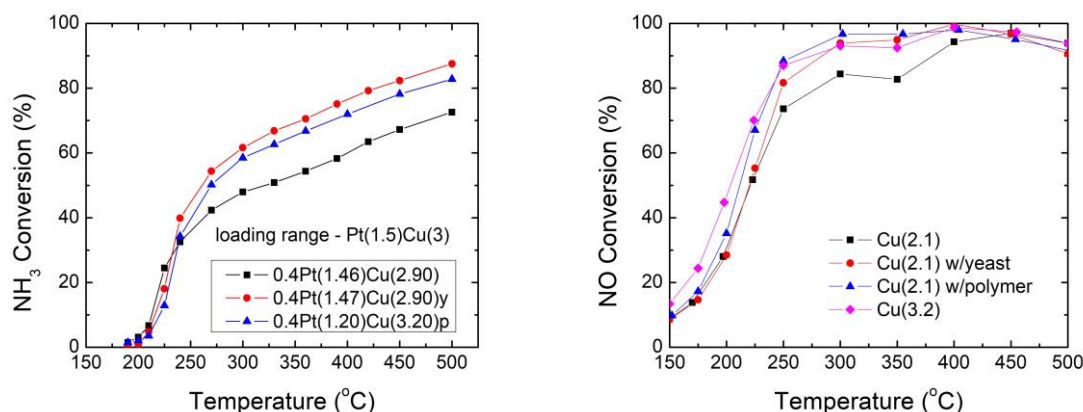


Figure 2. [Left] – NH₃ conversion as a function of temperature (steady state). Reactants: NH₃ = 500 ppm, O₂ = 5% and balance Ar (GHSV = 332 k h⁻¹); [Right] – NO conversion as function of temperature (steady state). Reactants: NO and NH₃ 500 ppm each, O₂ = 5% and balance Ar (GHSV: 66kh⁻¹)

4. Conclusions

Significant enhancement in NH₃ conversion was achieved for ammonia slip catalysts while maintaining high N₂ selectivity. The improved ASC activity could be explained by the higher porosity generated by sacrificial agents, which was also demonstrated by a mathematical model.

References

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Keywords

Ammonia slip catalyst (ASC); selective catalytic reduction (SCR); monolith reactor; vehicle emission control