

Effect of Dry vs. Wet Grinding on the Catalytic Performance of Pyrite (FeS₂) in NaBH₄ Methanolysis for Hydrogen Generation

Isil Tokcan^{1*}, Derya Yildiz²

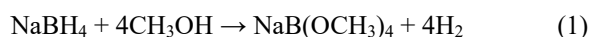
¹ Department of Mining Engineering, Eskisehir Osmangazi University, Eskisehir, 26040, Türkiye

² Department of Chemical Engineering, Eskisehir Osmangazi University, Eskisehir, 26040, Türkiye

Abstract. Catalysts play a critical role in hydrogen energy systems, and the development of low-cost, sustainable, and highly active alternatives remains a priority. In this study, pyrite (FeS₂) mineral prepared by dry and wet grinding was investigated as a catalyst for NaBH₄ methanolysis. At 30 °C, hydrogen generation rate (HGR) values of 2256 and 3221 mL·min⁻¹·gcat⁻¹ were determined for wet-ground (PW1) and dry-ground (PD1) samples, respectively. Characterization results revealed that dry grinding yields a higher BET specific surface area (1.23 vs. 0.61 m²/g), attributed to the deposition of iron oxyhydroxide species on pyrite surfaces during wet milling through galvanic interactions, which reduce accessible surface area and catalytic activity. Under optimised conditions (0.025 g catalyst, 0.125 g NaBH₄, 10 mL methanol, 60 °C), PD1 achieved an HGR of 19990 mL·min⁻¹·gcat⁻¹ with an activation energy of 38.07 kJ·mol⁻¹, demonstrating that dry grinding preserves chemically reactive fracture surfaces and enhances catalytic performance.

1. Introduction

Growing global energy demand and environmental concerns have intensified research into hydrogen as a clean energy carrier. Among chemical hydrides, NaBH₄ offers notable advantages including non-toxic and non-flammable nature, high stability, recyclability, and a theoretical H₂ storage capacity of up to 10.8 wt% [1]. In methanolysis, NaBH₄ reacts with methanol to release hydrogen according to Equation (1):



A catalyst is necessary to accelerate this reaction efficiently. With suitable catalysts, high-purity H₂ can be produced from NaBH₄ at room temperature [1]. Iron-containing catalysts have shown considerable activity in this context. Fe-B nanoparticles (Fe-B NPs/Ni foam) were supported on porous Ni foam. The catalyst exhibited an activation energy of 7.02 kJ·mol⁻¹ at 20–50°C [2]. Fe₃O₄, Fe₃O₄@SiO₂ and Fe₃O₄@SiO₂@NH₂ nanoparticles were found to be effective catalysts for the methanolysis reaction of NaBH₄. The reaction, which takes 30 minutes to complete without a catalyst, was completed in 16, 10, and 20 minutes, respectively, using Fe₃O₄, Fe₃O₄@SiO₂, and Fe₃O₄@SiO₂@NH₂ catalysts. Using Fe₃O₄@SiO₂@NH₂, a HGR of 13188 mL·min⁻¹·gcat⁻¹ and an Ea value of 24.4 kJ·mol⁻¹ were calculated in the temperature range of 258–318 K [3].

The use of catalysts, particularly those containing metals, is crucial for controlling and accelerating hydrogen production via the methanolysis of NaBH₄ due to their high reactivity and reaction rates; however, their application is limited by cost [4].

Pyrite (FeS₂), one of the most abundant metallic sulfide minerals in the Earth's crust, is the primary gangue mineral in complex sulfide ores; its content in porphyry copper ores ranges from 0.3% to 14.9% [5]. It is commonly found alongside sphalerite, chalcopyrite, galena, and gold-bearing minerals [6]. An important factor affecting the surface properties of pyrite is the grinding environment and the galvanic interactions that occur between minerals [7]. The grinding environment employed in catalyst preparation therefore directly determines the surface chemistry and catalytic potential of pyrite through distinct mechanochemical and electrochemical processes.

Grinding not only reduces particle size but also alters physicochemical surface properties through mechanochemical activation [8]. Secondary processes such as agglomeration and recrystallisation may partially offset these gains over extended milling times [9].

The grinding environment, whether dry or wet, plays a decisive role in determining the extent and nature of these changes. Dry grinding consistently produces deeper structural distortions than wet grinding at equivalent energy input, as the absence of water allows freshly fractured, high-energy surfaces to be preserved rather than immediately passivated. In wet grinding, the aqueous medium promotes surface hydroxylation, which passivates reactive sites and limits the extent of mechanochemical activation [10]. For sulfide minerals, galvanic interactions between steel media and pyrite release Fe²⁺ and Fe³⁺ ions that hydrolyze and precipitate as iron oxyhydroxide species on mineral surfaces, reducing chemical activity [11], [12], [13]. Dry grinding

* Corresponding author: e-mail address here

eliminates this electrochemical pathway, preserving mechanically activated fracture surfaces [10].

In this study, pyrite ore was ground by both methods and used as a catalyst in NaBH_4 methanolysis. The surface properties of samples obtained under different grinding conditions were characterized, and the effect on hydrogen production performance was experimentally determined. Although the effects of grinding environment on particle size and surface morphology are well established in ore processing, its impact on catalytic performance in H_2 production remains insufficiently addressed. This study evaluates the potential of natural waste ores as a low-cost and sustainable catalyst alternative.

2. Experimental

2.1 Characterization Methods

The surface areas of the catalysts were calculated using the BET (Brunauer, Emmett and Teller) equation in the relative pressure range of 0.01–1. Crystal structures were determined by XRD analysis using a PANalytical Empyrean device with $\text{Cu-K}\alpha$ radiation ($\lambda = 1.5406 \text{ \AA}$) over $2\theta = 10^\circ$ – 90° .

2.2. Materials and Chemicals

NaBH_4 (99% purity, AFG Bioscience) and methanol (Emsure®) were used without further purification.

2.3. Grinding Methods

Pyrite samples from Central Anatolia were crushed, ground with an agate mortar and pestle, and dry-sieved to below $425 \text{ }\mu\text{m}$. To minimise oxidation, material was sealed and stored at -18°C . For each experiment, 5 g of pyrite was ground in a stainless steel mill ($\varnothing 40 \times 75 \text{ mm}$) with 30 steel balls (6 mm diameter) mounted on a Retsch sieve shaker. For wet grinding, 5 ml of distilled water was added. Milling times were established from preliminary experiments to yield comparable product d_{50} , 10 min for dry and 6 min for wet grinding. Particle size distributions were measured by laser diffraction (Malvern Mastersizer Hydro 2000 MU).

2.4. Hydrogen Production

Dry- and wet-ground pyrite samples were designated PD1 and PW1, respectively, and used as catalysts in NaBH_4 methanolysis. Specific amounts of NaBH_4 and catalyst were placed in a sealed flask in a water bath; methanol at the same temperature was then injected. Released H_2 displaced water in a buret, and the gas volume was recorded over time. The hydrogen generation rate (HGR, $\text{mL} \cdot \text{min}^{-1} \cdot \text{g}_{\text{cat}}^{-1}$) was calculated from the initial slope of a polynomial fit to the volume–time data using Equation (2):

$$\frac{1}{W_{\text{cat}}} \left(\frac{dV_{\text{H}_2}}{dt} \right) = r_{\text{H}_2} \quad (2)$$

Experiments were conducted under identical conditions for PD1 and PW1. For the superior catalyst, the effects of catalyst amount, NaBH_4 amount, and temperature on HGR were then systematically investigated.

3. Results and Discussion

3.1. Characterization of Catalyst

XRD analyses were performed for both samples using $\text{Cu K}\alpha$ radiation ($\lambda = 1.5406 \text{ \AA}$) over approximately 5° – 90° (2θ). As shown in Figure 1, characteristic diffraction peaks of both samples are consistent with the pyrite phase (ICDD 00-042-1340, FeS_2). Peaks at approximately $2\theta = 28.5^\circ$, 33.0° , 37.0° , 40.8° , 47.5° , 56.3° , and 61.3° correspond to crystal planes (111), (200), (210), (211), (220), (311), and (222). The absence of secondary phase peaks indicates high purity in both samples.

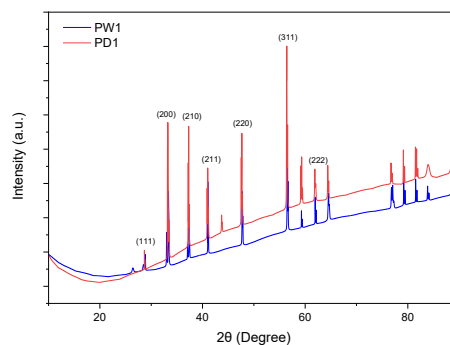


Figure 1. XRD patterns of pyrite samples

Crystallite sizes were approximately calculated using the Scherrer equation ($D = K\lambda / \beta \cos\theta$). In the calculations, $K = 0.9$ and $\lambda = 1.5406 \text{ \AA}$ were used, with the peak of highest density, approximately 56.3° (plane 311), used as a reference. Based on the approximate values obtained from the peak widths (FWHM), the crystallite size in the dry-ground sample is approximately in the range of 40–50 nm, while in the wet-ground sample this value decreases to the range of 20–30 nm. This result shows that wet grinding significantly reduces the crystallite size. The peaks appear sharper and more intense in the dry-ground (PD1) sample. This indicates that the crystal structure is better preserved and the crystallite size is larger. In the wet-ground sample (PW1), it was observed that the peaks were wider and their intensities were relatively reduced. The presence of a liquid medium during wet grinding causes interparticle collisions to be more effective and homogeneous, leading to distortions in the crystal lattice and smaller crystallite sizes. However, despite the smaller crystallite size observed in the wet-ground sample, its catalytic activity is lower than that of the dry-ground sample.

The surface properties of two different pyrite samples prepared using dry and wet grinding methods were investigated using the Brunauer–Emmett–Teller (BET) method. The grinding process is a critical parameter that significantly affects not only the crystal structure of minerals but also their surface area and pore structure. A regular increase in the amount of adsorbed gas was observed for both samples as the relative pressure increased. It is evident that both samples possess a mesoporous structure. It was observed that the dry-ground sample adsorbed a higher amount of gas compared to the wet-ground sample. This can be explained by effects such as surface rearrangement, agglomeration, or partial pore

blockage that occur during the grinding process in a wet environment. This finding confirms that the dry grinding process provides a higher specific surface area or a more developed pore structure.

BET analysis confirmed that both samples exhibit Type IV isotherm behavior (IUPAC), indicating mesoporous structures. PD1 has a BET surface area of 1.228 m²/g compared to 0.607 m²/g for PW1. Since particle size distributions under both conditions are nearly identical (Figure 2), the difference in surface area cannot be attributed to comminution efficiency. Rather, galvanic interactions during wet grinding precipitate iron oxyhydroxide species on freshly formed pyrite surfaces [11], [13], blocking accessible sites for N₂ adsorption and reducing the measured BET surface area. In dry grinding, the absence of an aqueous medium prevents such surface precipitation, preserving clean and reactive fracture surfaces. This interpretation is consistent with previous reports showing that wet-ground pyrite surfaces exhibit higher heterogeneity due to iron hydroxide and oxide deposits, which can be removed by EDTA washing to reveal the underlying sulfur-enriched surface [14].

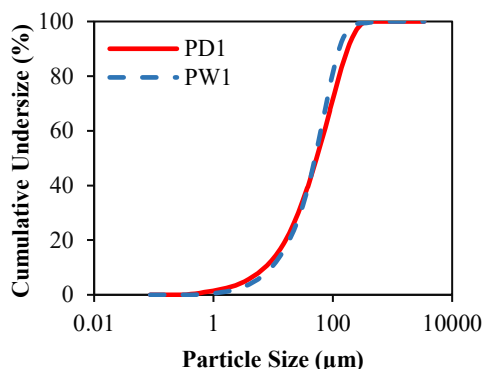


Figure 2. Particle size distributions of ground pyrite samples

3.2. Hydrogen Production Results

The time-dependent hydrogen production rates of the PD1 and PW1 catalysts were compared using 0.05 g of catalyst, 0.125 g of NaBH₄, 10 mL of methanol, and at 30°C. Both catalysts produced hydrogen at the theoretical hydrogen volume. However, the highest hydrogen production rate (HGR) was achieved with the PD1 catalyst. PD1 yielded an HGR of 3221 mL·min⁻¹·g_{cat}⁻¹, while PW1 yielded 2256 mL·min⁻¹·g_{cat}⁻¹. The effects of reaction parameters on the hydrogen production rate were investigated using the catalyst exhibiting higher activity.

The effect of catalyst amount was investigated at 30 °C using 0.125 g NaBH₄ in 10 mL methanol with 0.025, 0.05, 0.125, and 0.250 g catalyst (Figure 3). Although increasing catalyst amount raises the absolute reaction rate, HGR (calculated per gram of catalyst) was highest at the lowest catalyst amount (0.025 g). HGR values of 5136 mL·min⁻¹·g_{cat}⁻¹, 3221 mL·min⁻¹·g_{cat}⁻¹, 1381 mL·min⁻¹·g_{cat}⁻¹, and 1074 mL·min⁻¹·g_{cat}⁻¹ were obtained for catalyst amounts of 0.025 g, 0.05 g, 0.125 g, and 0.250 g, respectively. Based on these findings, 0.025 g was determined to be the optimal catalyst amount to balance reaction efficiency and catalyst quantity in the methanolysis of NaBH₄.

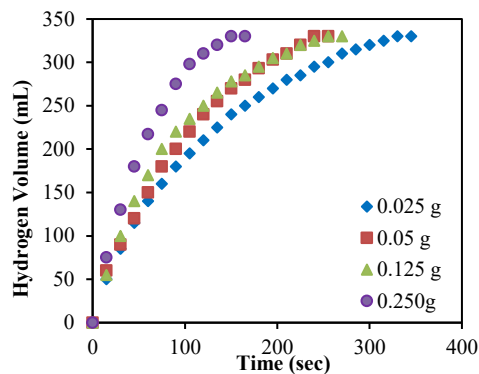


Figure 3. Effect of catalyst amount

To investigate the effect of the NaBH₄ amount, methanolysis reactions were carried out using 0.05 g, 0.100 g, 0.125 g, and 0.150 g of NaBH₄. These experiments were conducted in 10 mL of methanol solution in the presence of 0.025 g of catalyst at 30 °C. The results are presented in Figure 4. HGR values of 2207, 3855, 5136, and 10503 mL·min⁻¹·g were obtained, respectively. 0.125 g of NaBH₄ was considered the most suitable reactant amount.

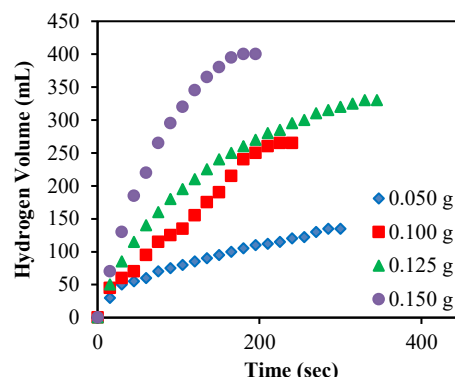


Figure 4. Effect of NaBH₄ amount

The effect of temperature was investigated at 25, 30, 40, 50, and 60 °C with 0.025 g catalyst, 0.125 g NaBH₄, and 10 mL methanol (Figure 5). HGR values increased with temperature: 2634, 5136, 11353, 12835, and 19990 mL·min⁻¹·g_{cat}⁻¹ at 25, 30, 40, 50, and 60 °C, respectively. Activation energy was calculated from the Arrhenius equation (Equations 3):

$$\ln k = \ln A - E_a/RT \quad (3)$$

Here, *k* represents the reaction rate constant, *T* the Arrhenius constant, *E_a* the activation energy, *R* the gas constant, and *T* the absolute temperature in Kelvin.

E_a is calculated as 38.07 kJ·mol⁻¹. This relatively low *E_a* indicates that the catalyst may allow for efficient hydrogen production under suitable conditions by reducing the energy barrier for the methanolysis reaction of NaBH₄. Under optimised conditions (0.025 g catalyst, 0.125 g NaBH₄, 10 mL methanol, 60 °C), PD1 achieved an HGR of 19990 mL·min⁻¹·g_{cat}⁻¹. This compares favourably with pyrite modified with polyethylenimine (PEI), which yielded 2883 mL·min⁻¹·g_{cat}⁻¹ [15]; CS/FeS₂ composites, which achieved 8000 mL·min⁻¹·g_{cat}⁻¹ at 25

°C [16]; and Fe₃O₄/FeS₂ hybrid structures at 8480 mL·min⁻¹·g_{cat}⁻¹ at 20 °C [17].

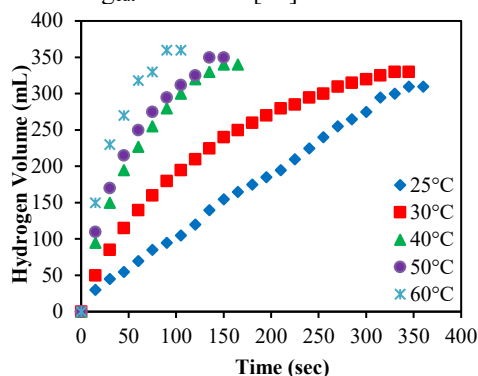


Figure 5. Effect of temperature

4. Conclusions

This study demonstrated the feasibility of using dry- and wet-ground pyrite (FeS₂) as a catalyst for NaBH₄ methanolysis. At 30 °C, dry-ground PD1 significantly outperformed wet-ground PW1.

The superior performance of dry-ground pyrite is attributed to the preservation of chemically reactive, high-energy fracture surfaces in the absence of aqueous passivation and galvanic interactions with steel grinding media. Characterization confirmed that the grinding environment alters mineral surface properties and that these changes directly influence catalytic performance. These findings establish the grinding environment as a critical parameter in mineral-based catalyst preparation for hydrogen generation. Furthermore, naturally occurring minerals offer a low-cost and earth-abundant alternative to synthetic catalyst systems. From a mineral processing perspective, dry grinding presents an additional advantage for sustainable operations in water-scarce regions.

Acknowledgement

This study has been funded by the Scientific Research Foundation, Eskisehir Osmangazi University, under grant numbers FHD-2025-3585.

References

- [1] Y. Wu *et al.*, "Synthesis of novel activated carbon-supported trimetallic Pt–Ru–Ni nanoparticles using wood chips as efficient catalysts for the hydrogen generation from NaBH₄ and enhanced photodegradation on methylene blue," *International Journal of Hydrogen Energy*, Aug. 2022, doi: 10.1016/j.ijhydene.2022.07.152.
- [2] J. D. Ocon, T. N. Tuan, Y. Yi, R. L. De Leon, J. K. Lee, and J. Lee, "Ultrafast and stable hydrogen generation from sodium borohydride in methanol and water over Fe–B nanoparticles," *Journal of Power Sources*, vol. 243, pp. 444–450, Dec. 2013, doi: 10.1016/j.jpowsour.2013.06.019.
- [3] N. Sahiner and S. B. Sengel, "Various amine functionalized halloysite nanotube as efficient metal free catalysts for H₂ generation from sodium borohydride methanolysis," *Applied Clay Science*, vol. 146, pp. 517–525, Sep. 2017, doi: 10.1016/j.clay.2017.07.008.
- [4] J. Yu *et al.*, "Ultrafine ruthenium-iridium alloy nanoparticles well-dispersed on N-rich carbon frameworks as efficient hydrogen-generation electrocatalysts," *Chemical Engineering Journal*, vol. 417, p. 128105, Aug. 2021, doi: 10.1016/j.cej.2020.128105.
- [5] C. Greet, J. Kinal, and G. Small, "The influence of grinding chemistry on chalcopyrite/pyrite selectivity for porphyry copper ores," presented at the IMPC 2016, Québec, Canada: Canadian Institute of Mining, Metallurgy and Petroleum.
- [6] C. L. Jiang, X. H. Wang, B. K. Parekh, and J. W. Leonard, "The surface and solution chemistry of pyrite flotation with xanthate in the presence of iron ions," *Colloids and Surfaces A: Physicochemical and Engineering Aspects*, vol. 136, no. 1–2, pp. 51–62, Apr. 1998, doi: 10.1016/S0927-7757(97)00250-1.
- [7] G. Huang, S. Grano, and W. Skinner, "Galvanic interaction between grinding media and arsenopyrite and its effect on flotation: Part II. Effect of grinding on flotation," *International Journal of Mineral Processing*, vol. 78, no. 3, pp. 198–213, Feb. 2006, doi: 10.1016/j.minpro.2005.10.009.
- [8] P. Baláz, *Mechanochemistry in Nanoscience and Minerals Engineering*. Berlin, Heidelberg: Springer Berlin Heidelberg, 2008. doi: 10.1007/978-3-540-74855-7.
- [9] P. Baláz, "Mechanical activation in hydrometallurgy," *International Journal of Mineral Processing*, vol. 72, no. 1–4, pp. 341–354, Sep. 2003, doi: 10.1016/S0301-7516(03)00109-1.
- [10] S. C. Chelgani, M. Parian, P. S. Parapari, Y. Ghorbani, and J. Rosenkranz, "A comparative study on the effects of dry and wet grinding on mineral flotation separation—a review," *Journal of Materials Research and Technology*, vol. 8, no. 5, pp. 5004–5011, Sep. 2019, doi: 10.1016/j.jmrt.2019.07.053.
- [11] M. K. Yelloji Rao and K. A. Natarajan, "Effect of galvanic interaction between grinding media and minerals on sphalerite flotation," *International Journal of Mineral Processing*, vol. 27, no. 1–2, pp. 95–109, Sep. 1989, doi: 10.1016/0301-7516(89)90008-2.
- [12] J. D. Pease, D. C. Curry, and M. F. Young, "Designing flotation circuits for high fines recovery," *Minerals Engineering*, vol. 19, no. 6–8, pp. 831–840, May 2006, doi: 10.1016/j.mineng.2005.09.056.
- [13] A. Rabieh, B. Albijanic, and J. J. Eksteen, "Influence of grinding media and water quality on flotation performance of gold bearing pyrite," *Minerals Engineering*, vol. 112, pp. 68–76, Oct. 2017, doi: 10.1016/j.mineng.2017.07.010.
- [14] S. Xu, M. Zanin, W. Skinner, and S. Brito E Abreu, "Surface chemistry of oxidised pyrite during grinding: EDTA extraction analysis," *Minerals Engineering*, vol. 160, p. 106683, Jan. 2021, doi: 10.1016/j.mineng.2020.106683.
- [15] E. Inger, S. Demirci, M. Can, A. K. Sunol, G. Philippidis, and N. Sahiner, "PEI MODIFIED natural sands of Florida as catalysts for hydrogen production from sodium borohydride dehydrogenation in methanol," *Int J Energy Res*, vol. 45, no. 3, pp. 4048–4067, Mar. 2021, doi: 10.1002/er.6060.
- [16] N. A. Azab, S. M. Syam, A.-A. M. El-Sharkawy, W. A. A. Bayoumy, K. A. Soliman, and M. M. Mohamed, "Photoelectrochemical, magneto-enhanced hydrogen evolution, and methanolysis on biomass carbon/FeS₂ composites," *Journal of Environmental Chemical Engineering*, vol. 14, no. 2, p. 121681, Apr. 2026, doi: 10.1016/j.jece.2026.121681.
- [17] M. Alshammari *et al.*, "Hydrogen catalytic performance of hybrid Fe₃O₄/FeS₂/g-C₃N₄ nanocomposite structures," *Diamond and Related Materials*, vol. 138, p. 10214, Oct. 2023, doi: 10.1016/j.diamond.2023.110214.