A Novel Process for Blue Hydrogen Production with Molten Carbonate Fuel Cell CO2 Capture

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Abstract

H2 production via steam methane reforming is a mature and cost-effective technology. However, carbon capture and storage is required to decrease its CO2 emissions. The adoption of molten carbonate fuel cells as means to capture CO2 from flue gases is attracting scientific interest thanks to their inherent thermodynamic advantage of separating CO2 while producing electricity. This study investigates and benchmarks the performance of an H2 production plant equipped with molten carbonate fuel cell for post-combustion CO2 capture, by proposing a novel configuration where the cell anode is fed with the carbon-rich off-gas from the H2 separation unit. It emerges that the process can achieve higher capture rates than the reference solvent-based plant: 85-90 % with single cell, 95 % with two-stage cell. Moreover, recycling the carbon-rich off gas to the anode allows for smaller cell area, and potentially lower H2 production costs compared to the benchmark.

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**Keywords**: Steam methane reformer, Molten carbonate fuel cell, Carbon dioxide capture, Process simulation, Techno-economic modelling.

* 1. Introduction

H2 is expected to become a key player in the decarbonisation challenge (van der Spek et al., 2022). The production of H2 from fossil fuels with CO2 capture is key to enable large scale production and will be complementary to electrolysis till the electric grid is decarbonised, provided that CO2 capture is performed according to state-of-the-art and CH4 fugitive losses are minimised (Bauer et al., 2022; Pettersen et al., 2022). This work focusses on H2 production from steam methane reforming (SMR) of natural gas (NG), which is a mature and cost-effective technology (IEAGHG, 2017), coupled with molten carbonate fuel cell (MCFC) for post-combustion CO2 capture.

In the literature, post-combustion CO2 capture processes based on MCFC for H2 plants and other emitters consider NG as fuel for the fuel cell (Consonni et al., 2021). This study proposes a novel configuration (d’Amore et al., 2023), which exploits part of the off-gas from H2 purification unit as fuel to the MCFC, instead of NG. This configuration keeps a carbon-richer fuel on the MCFC anode side and reduces the flow rate of CO2 in the SMR to be separated by the MCFC (thus, its area) for a given CO2 capture rate, with significant beneficial effects in the overall techno-economic performance. Building upon the performance of the novel off-gas feed configuration, it is also assessed how a multi-stage cell configuration with inter-cooling would further improve the process (Spinelli et al., 2014), as it helps decreasing the air dilution at the MCFC cathode inlet and enhances the CO2 separation efficiency.

* 1. Methodology

The plants were modelled and simulated in Aspen Plus software by using the Peng-Robinson equation of state, according to the technical assumptions summarised in d’Amore et al. (2023) (Table 1). All chemical reactors were simulated at chemical equilibrium, while the MCFC performance is described through a 0-D model of the polarisation curve taken from Barckholtz et al. (2022).

The reference standalone SMR without CO2 capture is designed to produce 100,000 Nm3/h of H2 (299.5 MWLHV), comprising high temperature water-gas shift (WGS), pressure swing adsorption (PSA), steam cycle (set at 485 °C at 100 bar), and low pressure (LP) steam export (at 6 bar) (Figure 1a). This plant is characterised by an NG-to-H2 efficiency of 73.5 % and specific CO2 emissions of 9.29 kg of CO2/kg of H2, being the net electric and thermal power outputs equal to 10.4 MWel and 23.2 MWth, respectively. The SMR with post-combustion CO2 capture with monoethanolamine (MEA) is designed for a CO2 capture rate of 90 % and a specific heat demand of 3.57 MJth/kg of captured CO2 (Figure 1b). This plant is considered as benchmark case for performance and costs comparison with MCFC-based CO2 capture.

In the NG-based MCFC (i.e., NGF plant) the SMR flue gases are sent to the MCFC cathode for CO2 separation. A CO2 lean stream is produced at the cathode residue and emitted to the atmosphere (Figure 1c). The MCFC anode is fed with pre-reformed NG. The anode residue is sent to a WGS converter. The shifted syngas stream is sent to the low-temperature phase-change purification unit (CPU) to produce a high-purity CO2 stream and a flow rate that is recycled to the PSA unit downstream the SMR. Differently, in the off-gas-based MCFC (i.e., OGF plant) the MCFC anode is fed with PSA off-gas (Figure 1d). This configuration keeps the carbon-rich fuel on the MCFC anode side and reduces the flow rate of CO2 in the SMR to be separated by the MCFC (therefore, its area) for a given overall CO2 capture rate. An additional case (i.e., OGF-2) involves the adoption of two cells in series with inter-cooling to decrease the air dilution at the cathode inlet and enhance the CO2 separation efficiency for a given cell potential.

Table 1. Summary of the main input data.

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| Plant | Component | Parameter | Value | Unit |
| SMR | Pre-reformer | Steam-to-carbon | 3.4 | mol/mol |
|  | Reformer | Outlet temperature | 890 | °C |
|  | PSA | H2 recovery | 90 | % |
|  | LP steam | Pressure | 6 | bar |
|  | HP steam | Pressure/temperature | 100/485 | bar/°C |
| MEA | CO2 separation | Efficiency | 90 | % |
|  | CO2 separation | Reboiler duty | 3.57 | GJ/t CO2 |
| MCFC | Cathode | Inlet temperature | 575 | °C |
|  | Cathode | Outlet temperature | 645 | °C |
|  | Cathode | CO2 outlet concentration | 1 | %mol |
|  | Pre-reformer | Inlet temperature | 600 | °C |
|  | Pre-reformer | Steam-to-carbon | 2.1 | mol/mol |
|  | Anode | Inlet temperature | 600 | °C |
|  | Anode | Outlet temperature | 645 | °C |

Immagine che contiene testo, diagramma, Carattere, Piano

Descrizione generata automaticamente

Figure 1. Simplified plant schemes: (a) SMR, (b) SMR with MEA, (c) NGF, and (d) OGF.

* 1. Results

Even though MCFC-based plants consume more NG with respect to the standalone SMR (between +8 % and +26 %), they also generate a larger low-carbon electricity output (Table 2). Plus, MCFC-based OGF and OGF-2 cases show a better performance compared to MEA solvent-based capture system in a wide range of NG and electricity prices. OGF appears superior to NGF, being the former characterised by higher carbon capture rate (90 % against 85 %), higher H2 production efficiency (68 % against 59 %), lower specific energy consumption per unit of CO2 avoided (0.5 against 1.1 MJ/kg of CO2), and a significantly lower cell area (-43 %). This is due to the higher carbon intensity of the off-gas feed to the OGF cell anode, compared to the NG exploited in the NGF case, which allows reducing the flow rate of CO2 to be separated by the MCFC for a given CO2 capture rate. OGF-2 is a particularly competitive configuration, as it can achieve 95 % carbon capture rate with a smaller cell area than OGF (-19 %). This is due to the inter-cooling between cells, which allows reducing the CO2 dilution resulting from the excess air to be mixed with the flue gas to control the MCFC temperature.

Table 2. Technical performance results.

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
|  | SMR | MEA | NGF | OGF | OGF-2 |
| Cell 1 potential [V] | - | - | 0.70 | 0.70 | 0.65 |
| Cell 2 potential [V] | - | - | - | - | 0.60 |
| Util. factor [%] | - | - | 75.0 % | 75.0 % | 70.0 % |
| CO2 util. factor [%] | - | - | 81.7 % | 77.5 % | 87.1 % |
| Total cell area [m2] | - | - | 73123 | 41615 | 23605 |
| NG plant inlet [MWLHV] | 407.3 | 407.3 | 512.4 | 442.2 | 439.4 |
| PSA off-gas [MWLHV] | 97.1 | 97.1 | 90.8 | 95.0 | 94.6 |
| Electricity outlet [MWel] | 10.4 | -12.8 | 59.1 | 22.1 | 19.8 |
| Steam outlet [MWth] | 23.2 | 0.0 | 21.5 | 24.6 | 26.2 |
| Spec. emis. [kgCO2/kgH2] | 9.29 | 0.93 | 1.75 | 0.98 | 0.50 |
| H2 prod. eff. [%] | 73.5 % | 73.5 % | 58.5 % | 67.7 % | 68.2 % |
| Carbon capt. Rate [%] | 0.0 % | 90.0 % | 85.0 % | 90.3 % | 95.0 % |

The economic analysis is based on the assumptions reported in d’Amore et al. (2023). The plants have equivalent operating hours of 8400 h/year, being the electricity and natural gas prices equal to 60 €/MWh and 6 €/GJ, respectively. The results show that OGF and OGF-2 plants exhibit H2 production costs (1.9-2.2 €/kg of H2) that are lower than NGF (2.3-2.6 €/kg of H2) and than SMR with conventional post-combustion CO2 capture (2.2-2.3 €/kg of H2). The sensitivity analyses on key economic parameters (e.g., carbon tax, NG cost, electricity price) did not affect the main outcome, i.e., the good economic performance of OGF and OGF-2 (d’Amore et al., 2023). Contrary to the NGF case, the OGF one (and especially the 2-stage configuration) emerges as cost competitive with conventional solvent-based post-combustion capture in the entire range of values explored in the sensitivities.

* 1. Conclusions

This study highlights the potential of molten carbonate fuel cells (MCFCs) as post-combustion CO2 capture systems in blue H2 plants, if fed with off-gas from H2 purification unit as fuel. The resulting CO2 capture rate is found equal to 90 % for the single cell configuration and equal to 95 % for the multi-stage cell configuration, against 85 % in the case of natural gas-based anode feed. H2 production costs are in the range of 1.9-2.2 €/kg of H2, therefore lower than a traditional natural gas anode feed (2.3-2.6 €/kg H2), and competitive with solvent-based post-combustion capture (2.2-2.3 €/kg of H2).

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