

H₂S Removal in Biogas by Direct Catalytic Oxidation to Sulphur on V₂O₅/CeO₂ Catalysts

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The direct and selective partial H₂S oxidation to elemental sulphur at low temperature may be an interesting alternative to the traditional methods of H₂S abatement if an active and selective catalyst is available.

In our previous works, a screening of vanadium-based catalysts supported on the metal oxide (V₂O₅-TiO₂, V₂O₅-CeO₂, V₂O₅-CuFe₂O₄) was performed in the range of temperature 50-250 °C; among all the catalysts investigated, the V₂O₅/CeO₂ catalyst has showed the better catalytic performance in terms of H₂S conversion (>95 %) and a low SO₂ selectivity (~13 %) at T= 250 °C.

Based on these promising results, further investigations on V₂O₅/CeO₂ catalyst were performed to investigate the influence of the inlet concentration of H₂S (250-1000 ppm), the gas hourly space velocity (GHSV=15,000-45,000 h⁻¹) and the molar feed ratio (O₂/H₂S=0.4-0.5) in order to minimize the selectivity of the system to SO₂.

Preliminary results relevant to the effect of the gas hourly space velocity and the inlet concentrations of H₂S, showed that they did not contribute to reduce significantly the SO₂ selectivity, while interesting result in terms of SO₂ selectivity was obtained with a sub-stoichiometric feed ratio (O₂/H₂S = 0.4), for which it is resulted drastically reduced from 13 % to 4 % without any significant reduction of the H₂S and O₂ conversions.

From these good results, future works will be performed to investigate the effect of vanadium load by studying samples in the range 2.55-10 %wt in order to determine the optimal catalyst formulation and operative conditions to obtain a very high H₂S conversion and the SO₂ selectivity minimization.

1. Introduction

Biogas generated from anaerobic digestion processes is a clean and environmentally friendly renewable fuel. Due to the particular composition, biogas can be used in a large number of applications where it's expected the utilization of the natural gas: direct generation of heat (industrial boilers), production of energy and heat (internal combustion engines, gas turbines).

In addition, in these last years, the attention is also focused on the possibility to use the biogas for energy production in unconventional systems as the molten carbonate fuel cells.

The main real limitation to the utilization of the biogas as fuel for MCFC is represented by the poisoning of the anode, of the electrolyte, and the deactivation of catalyst oxidation sites by sulphur based compounds (H₂S, COS) that are always presents in biogas (Ciccoli et al., 2010). Even if present at low concentration level, they must be depressed at ppm values, because the sulphur content allowed in the MCFC is lower than 5 ppm. For these reasons, a H₂S clean-up stage must be considered (McPhail et al., 2009).

The most applied technique for the H₂S abatement in large scale plants is represented by the classical absorption process, characterized by high costs and a limited overall efficiency (Petersson et al., 2009, Zicari 2003).

For the small scale plant, a very interesting solution can be represented by the direct and selective H₂S catalytic oxidation to sulphur at low temperature.

Among all the catalysts investigated, the V₂O₅/CeO₂ catalyst has showed the better catalytic performance in terms of H₂S and O₂ conversion with a high sulphur yield and therefore it could be a good candidate for this reaction.

2. Experimental

The V₂O₅/CeO₂ catalyst with a nominal V₂O₅ load of 2.55 %wt was prepared by wet impregnation method. We started by aqueous solution of ammonium metavanadate (Aldrich), and powder ceria (Aldrich). This solution was placed on a heated plate until to water complete evaporation. After drying of the impregnated sample at 120 °C overnight, it was calcined at 400 °C for 3 h. For reaction test, catalyst has been reduced to the size 180-355 µm.

The catalyst prepared was also characterized by different techniques.

X-ray diffraction measures were performed with a Brucker D8 diffractometer with a monochromatic CuKα1 on the calcined catalyst before and after the catalytic tests and on the CeO₂ used as support.

Raman spectra were recorded in ambient conditions with a Spectroscopy Raman using as the excitation source an ion laser of 785 nm.

The catalytic tests were carried out in a fixed bed flow reactor, made of a pyrex glass tube 0.21 m long and a 0.02 m of internal diameter. The reactor is inserted in an electrical furnace equipped with a PID electronic temperature controller. The catalytic bed is located in the furnace in a selected region with an "isothermal" profile ($\pm 1^\circ\text{C}$).

A system of four-way valves allows to send the stream feed to the reactor, or in by-pass position, to send the stream feed to analysis. In the by-pass configuration, an independent MFC allows to send nitrogen to the reactor.

Preliminary tests were carried out at atmospheric pressure and GHSV of 15,000 h⁻¹, in the temperature range 50-250 °C, with 1000 ppm of H₂S, 500 ppm of O₂ and N₂ to balance.

The exhaust stream was analyzed by a quadrupole mass spectrometer equipped with a sulfur trap in order to follow all the reactants and the gaseous product at the reactor outlet.

The H₂S, O₂ conversions, and the SO₂ selectivity were calculated by using the following equations, by considering negligible the gas phase volume change:

$$x_{\text{H}_2\text{S}}, \% = (\text{ppm of H}_2\text{S reacted} / \text{ppm of H}_2\text{S fed}) \cdot 100$$

$$x_{\text{O}_2}, \% = (\text{ppm of O}_2 \text{ reacted} / \text{ppm of O}_2 \text{ fed}) \cdot 100$$

$$y_{\text{SO}_2}, \% = (\text{ppm of sulfur dioxide} / \text{ppm of hydrogen sulfide reacted}) \cdot 100$$

3. Results and Discussion

In the Figure 1 are compared XRD patterns of the CeO₂ support with catalyst V₂O₅/CeO₂ before and after the catalytic test.

All the samples exhibited the characteristic peaks of CeO₂; reflections cannot be detected for V₂O₅, likely due to the low metal loading (2.55% wt) and the good dispersion on the support (M.D. Soriano et al., 2009).

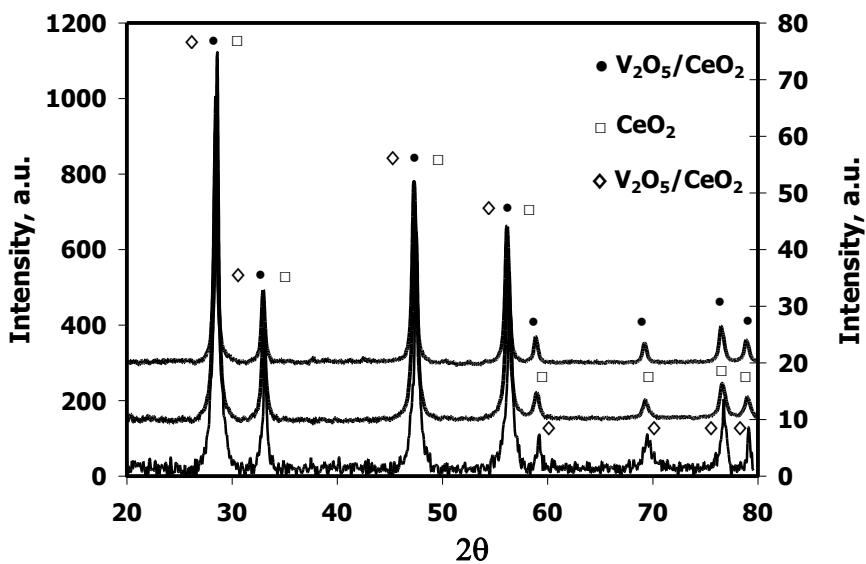


Figure 1: X-Ray diffraction patterns of CeO₂ and of the catalyst V₂O₅/CeO₂ before (•) and after the catalytic test (◊).

The Raman spectra of CeO₂ and V₂O₅/CeO₂ catalysts are shown in the Figure 2; the only peaks are relative to the CeO₂, revealing the highly dispersed state of vanadium.

A characteristic Raman peak of CeO₂ has been identified around 465 cm⁻¹ (Xiaodong Gu et al., 2006).

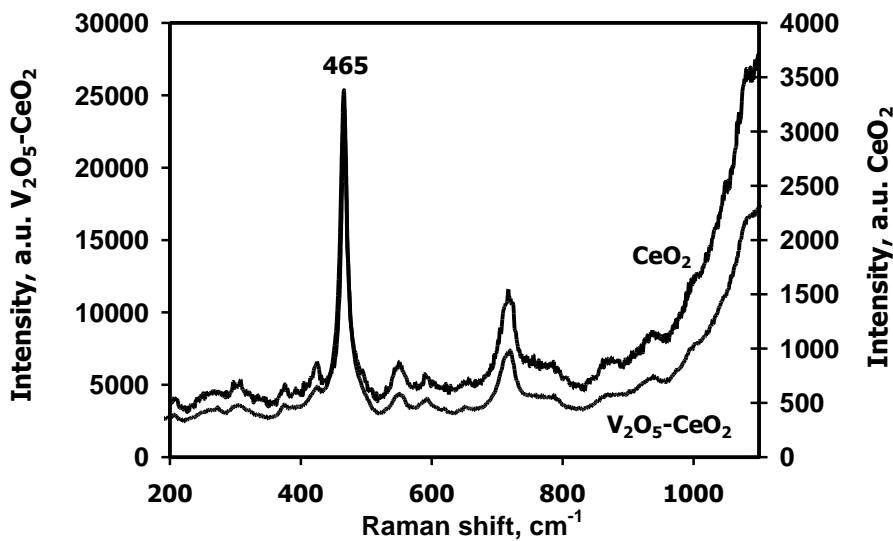


Figure 2: Raman spectra of CeO₂ and of the catalyst V₂O₅/CeO₂ before of the catalytic test.

In Figure 3 are reported results of catalytic activity test obtained at GHSV value of 15000 h⁻¹. The figure shows the behavior of the H₂S, O₂ conversions and SO₂ selectivity as function of temperature with an inlet H₂S concentration of 1000 ppm and an O₂/H₂S molar feed ratio of 0.5.

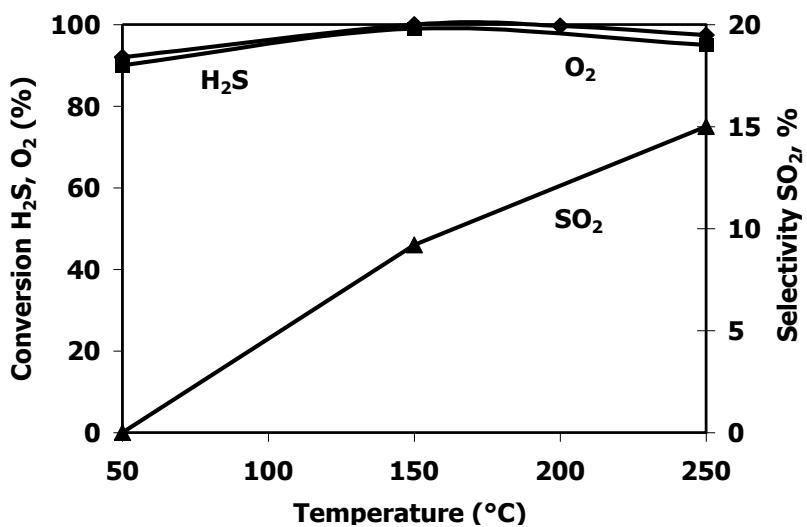


Figure 3: Conversion of H_2S , O_2 and SO_2 selectivity in the range $T=50-250$ °C

The experimental results show a very high H_2S and O_2 conversion, that is always higher than 90 %, and simultaneously a very low SO_2 production that increase with temperature, reaching the maximum selectivity value of 14 % at the highest temperature tested.

The results of catalytic activity of $V_2O_5-CeO_2$ catalyst at $T=250$ °C as function of time are reported in Figure 4.

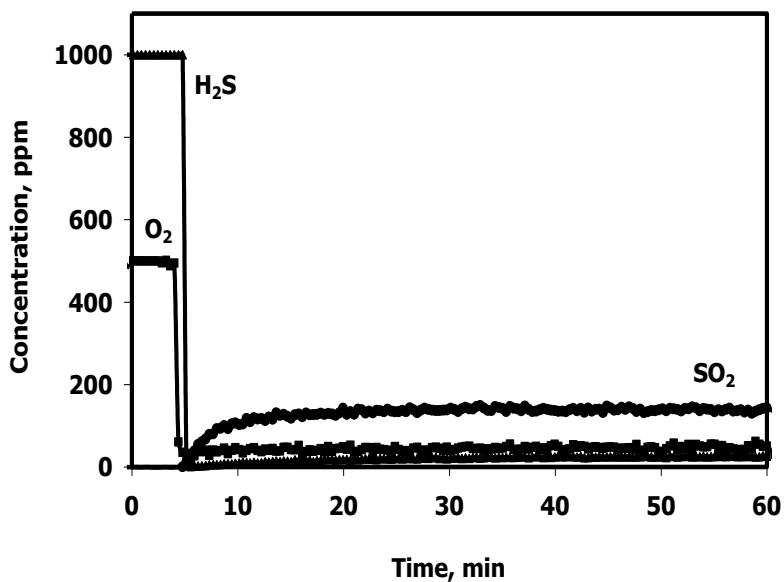


Figure 4: Stability test of $V_2O_5-CeO_2$ at $T=250$ °C (1000 ppm H_2S , $O_2/H_2S=0.5$).

The figure shows that the catalyst in the first hour of time on stream any deactivation is evident, and the catalyst exhibits a very high H₂S and O₂ conversion, but also a significant SO₂ concentration (140 ppm).

Further results concerning the effect of the gas hourly space velocity at constant inlet H₂S concentrations and O₂/H₂S molar feed ratio on the SO₂ selectivity are showed in Table 1, where despite the sensible change in the GHSV values, any significant variations of the H₂S, O₂ conversions and SO₂ selectivity are obtained.

Table 1: Effect of the gas hourly space velocity on the catalytic activity of V₂O₅/CeO₂ (T=250 °C, O₂/H₂S=0.5).

GHSV, h ⁻¹	X _{H₂S} , %	X _{O₂} , %	Y _{SO₂} , %
15,000	97	91	14
45,000	97	100	13

In Table 2 the effect of the inlet H₂S concentration (from 250 ppm to 1000 ppm) in the feed gas at constant temperature and O₂/H₂S molar feed ratio are reported in terms of H₂S conversion and SO₂ selectivity.

Table 2: Effect of the H₂S concentrations on the catalytic activity of V₂O₅/CeO₂ (T=250 °C, O₂/H₂S=0.5).

H ₂ S, ppm	O ₂ , ppm	X _{H₂S} , %	Y _{SO₂} , %
1000	500	98	14
500	250	98	17
250	125	100	26

In this case, the results reported in Table 2 show that there is a measurable effect of the initial concentration of H₂S in the gas supply only on the selectivity to SO₂.

Moreover, it is also evident that even significantly reducing the initial concentration of H₂S, is not found a similar reduction in the selectivity to SO₂.

In contrast with the very good results in terms of H₂S conversion, the SO₂ selectivity is not so bad when the O₂/H₂S feed ratio is 0.5. As a consequence, additional catalytic tests were performed at lower O₂/H₂S molar feed ratio values, and the relevant results are reported in Table 3, where a very good result in terms of SO₂ selectivity was obtained for the O₂/H₂S value of 0.4, for which the SO₂ selectivity results drastically reduced from 13 % to 4 % without any significant reduction of the H₂S and O₂ conversions.

Table 3: Effect of the feed ratio on the catalytic activity of V₂O₅/CeO₂ (T=250 °C, O₂/H₂S=0.5, GHSV=45,000 h⁻¹)

O ₂ /H ₂ S	X _{H₂S} , %	X _{O₂} , %	Y _{SO₂} , %
0.5	97	100	13
0.4	94	100	4

4. Conclusions

A vanadium-based catalyst supported on ceria with a nominal load of 2.55 %wt was prepared via impregnation method, and studied for the selective reaction of H₂S oxidation to sulfur. XRD and Raman characterization results showed that no signals relevant to the presence of isolated V₂O₅, suggesting that vanadium oxide is well dispersed on the CeO₂ surface. The V₂O₅/CeO₂ catalyst showed very good performances in terms of catalytic activity, stability and SO₂ selectivity. The effect of the gas hourly space velocity and the inlet concentrations of H₂S did not contribute to reduce significantly the SO₂ selectivity. An interesting result to reduce SO₂ selectivity from 14 % to 4 %, was obtained by decreasing the O₂/H₂S feed ratio from the stoichiometric one (O₂/H₂S = 0.5) to a slightly lower value (O₂/H₂S = 0.4).

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