



## H<sub>2</sub>S Removal in Biogas by Direct Catalytic Oxidation to Sulphur on V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> Catalysts

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The direct and selective partial H<sub>2</sub>S oxidation to elemental sulphur at low temperature may be an interesting alternative to the traditional methods of H<sub>2</sub>S abatement if an active and selective catalyst is available.

In our previous works, a screening of vanadium-based catalysts supported on the metal oxide (V<sub>2</sub>O<sub>5</sub>-TiO<sub>2</sub>, V<sub>2</sub>O<sub>5</sub>-CeO<sub>2</sub>, V<sub>2</sub>O<sub>5</sub>-CuFe<sub>2</sub>O<sub>4</sub>) was performed in the range of temperature 50-250 °C; among all the catalysts investigated, the V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> catalyst has showed the better catalytic performance in terms of H<sub>2</sub>S conversion (>95 %) and a low SO<sub>2</sub> selectivity (~13 %) at T= 250 °C.

Based on these promising results, further investigations on V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> catalyst were performed to investigate the influence of the inlet concentration of H<sub>2</sub>S (250-1000 ppm), the gas hourly space velocity (GHSV=15,000-45,000 h<sup>-1</sup>) and the molar feed ratio (O<sub>2</sub>/H<sub>2</sub>S=0.4-0.5) in order to minimize the selectivity of the system to SO<sub>2</sub>.

Preliminary results relevant to the effect of the gas hourly space velocity and the inlet concentrations of H<sub>2</sub>S, showed that they did not contribute to reduce significantly the SO<sub>2</sub> selectivity, while interesting result in terms of SO<sub>2</sub> selectivity was obtained with a sub-stoichiometric feed ratio (O<sub>2</sub>/H<sub>2</sub>S = 0.4), for which it is resulted drastically reduced from 13 % to 4 % without any significant reduction of the H<sub>2</sub>S and O<sub>2</sub> conversions.

From these good results, future works will be performed to investigate the effect of vanadium load by studying samples in the range 2.55-10 %wt in order to determine the optimal catalyst formulation and operative conditions to obtain a very high H<sub>2</sub>S conversion and the SO<sub>2</sub> selectivity minimization.

### 1. Introduction

Biogas generated from anaerobic digestion processes is a clean and environmentally friendly renewable fuel. Due to the particular composition, biogas can be used in a large number of applications where it's expected the utilization of the natural gas: direct generation of heat (industrial boilers), production of energy and heat (internal combustion engines, gas turbines).

In addition, in these last years, the attention is also focused on the possibility to use the biogas for energy production in unconventional systems as the molten carbonate fuel cells.

The main real limitation to the utilization of the biogas as fuel for MCFC is represented by the poisoning of the anode, of the electrolyte, and the deactivation of catalyst oxidation sites by sulphur based compounds (H<sub>2</sub>S, COS) that are always present in biogas (Ciccoli et al., 2010). Even if present at low concentration level, they must be depressed at ppm values, because the sulphur content allowed in the MCFC is lower than 5 ppm. For these reasons, a H<sub>2</sub>S clean-up stage must be considered (McPhail et al., 2009).

The most applied technique for the H<sub>2</sub>S abatement in large scale plants is represented by the classical absorption process, characterized by high costs and a limited overall efficiency (Petersson et al., 2009, Zicari 2003).

For the small scale plant, a very interesting solution can be represented by the direct and selective H<sub>2</sub>S catalytic oxidation to sulphur at low temperature.

Among all the catalysts investigated, the V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> catalyst has showed the better catalytic performance in terms of H<sub>2</sub>S and O<sub>2</sub> conversion with a high sulphur yield and therefore it could be a good candidate for this reaction.

## 2. Experimental

The V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> catalyst with a nominal V<sub>2</sub>O<sub>5</sub> load of 2.55 %wt was prepared by wet impregnation method. We started by aqueous solution of ammonium metavanadate (Aldrich), and powder ceria (Aldrich). This solution was placed on a heated plate until to water complete evaporation. After drying of the impregnated sample at 120 °C overnight, it was calcined at 400 °C for 3 h. For reaction test, catalyst has been reduced to the size 180-355 µm.

The catalyst prepared was also characterized by different techniques.

X-ray diffraction measures were performed with a Brucker D8 diffractometer with a monochromatic CuKα1 on the calcined catalyst before and after the catalytic tests and on the CeO<sub>2</sub> used as support.

Raman spectra were recorded in ambient conditions with a Spectroscopy Raman using as the excitation source an ion laser of 785 nm.

The catalytic tests were carried out in a fixed bed flow reactor, made of a pyrex glass tube 0.21 m long and a 0.02 m of internal diameter. The reactor is inserted in an electrical furnace equipped with a PID electronic temperature controller. The catalytic bed is located in the furnace in a selected region with an "isothermal" profile (±1°C).

A system of four-way valves allows to send the stream feed to the reactor, or in by-pass position, to send the stream feed to analysis. In the by-pass configuration, an independent MFC allows to send nitrogen to the reactor.

Preliminary tests were carried out at atmospheric pressure and GHSV of 15,000 h<sup>-1</sup>, in the temperature range 50-250 °C, with 1000 ppm of H<sub>2</sub>S, 500 ppm of O<sub>2</sub> and N<sub>2</sub> to balance.

The exhaust stream was analyzed by a quadrupole mass spectrometer equipped with a sulfur trap in order to follow all the reactants and the gaseous product at the reactor outlet.

The H<sub>2</sub>S, O<sub>2</sub> conversions, and the SO<sub>2</sub> selectivity were calculated by using the following equations, by considering negligible the gas phase volume change:

$$x_{\text{H}_2\text{S}}, \% = (\text{ppm of H}_2\text{S reacted} / \text{ppm of H}_2\text{S fed}) \cdot 100$$

$$x_{\text{O}_2}, \% = (\text{ppm of O}_2 \text{ reacted} / \text{ppm of O}_2 \text{ fed}) \cdot 100$$

$$y_{\text{SO}_2}, \% = (\text{ppm of sulfur dioxide} / \text{ppm of hydrogen sulfide reacted}) \cdot 100$$

## 3. Results and Discussion

In the Figure 1 are compared XRD patterns of the CeO<sub>2</sub> support with catalyst V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> before and after the catalytic test.

All the samples exhibited the characteristic peaks of CeO<sub>2</sub>; reflections cannot be detected for V<sub>2</sub>O<sub>5</sub>, likely due to the low metal loading (2.55% wt) and the good dispersion on the support (M.D. Soriano et al., 2009).

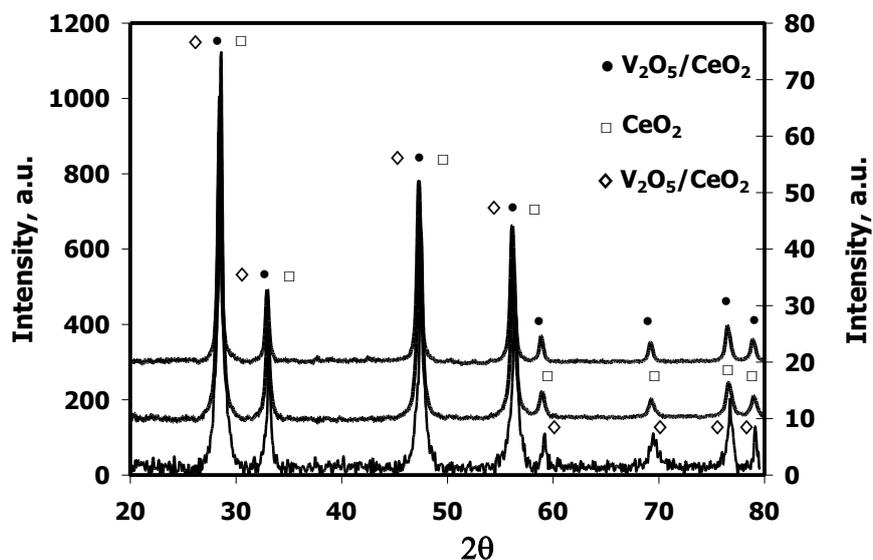


Figure 1: X-Ray diffraction patterns of  $\text{CeO}_2$  and of the catalyst  $\text{V}_2\text{O}_5/\text{CeO}_2$  before ( $\bullet$ ) and after the catalytic test ( $\diamond$ ).

The Raman spectra of  $\text{CeO}_2$  and  $\text{V}_2\text{O}_5/\text{CeO}_2$  catalysts are shown in the Figure 2; the only peaks are relative to the  $\text{CeO}_2$ , revealing the highly dispersed state of vanadium. A characteristic Raman peak of  $\text{CeO}_2$  has been identified around  $465\text{ cm}^{-1}$  (Xiaodong Gu et al., 2006).

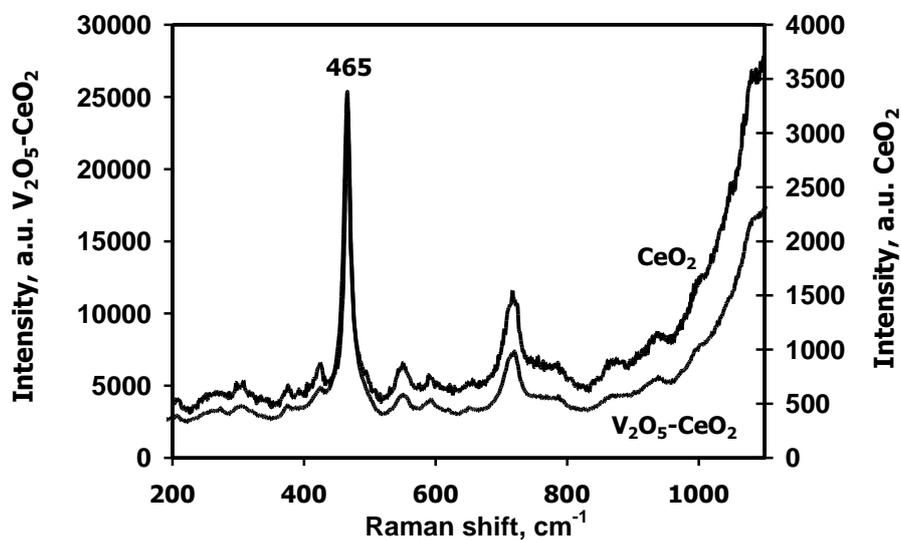


Figure 2: Raman spectra of  $\text{CeO}_2$  and of the catalyst  $\text{V}_2\text{O}_5/\text{CeO}_2$  before of the catalytic test.

In Figure 3 are reported results of catalytic activity test obtained at GHSV value of  $15000\text{ h}^{-1}$ . The figure shows the behavior of the  $\text{H}_2\text{S}$ ,  $\text{O}_2$  conversions and  $\text{SO}_2$  selectivity as function of temperature with an inlet  $\text{H}_2\text{S}$  concentration of 1000 ppm and an  $\text{O}_2/\text{H}_2\text{S}$  molar feed ratio of 0.5.

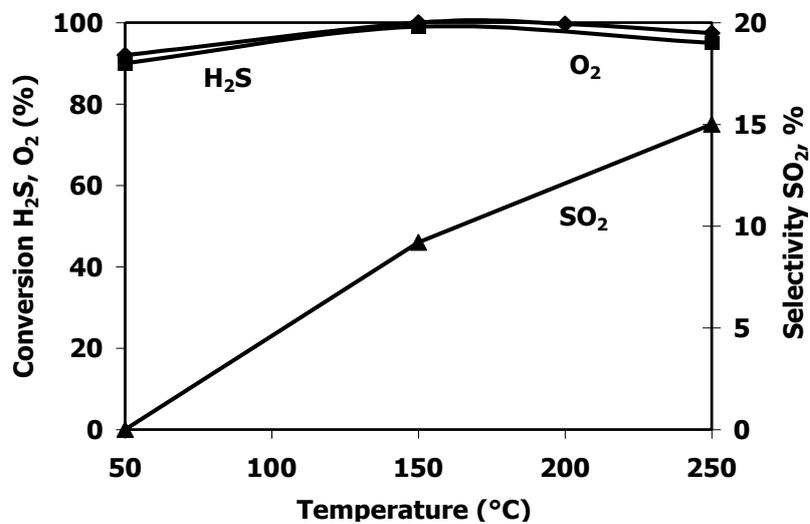


Figure 3: Conversion of H<sub>2</sub>S, O<sub>2</sub> and SO<sub>2</sub> selectivity in the range T=50-250 °C

The experimental results show a very high H<sub>2</sub>S and O<sub>2</sub> conversion, that is always higher than 90 %, and simultaneously a very low SO<sub>2</sub> production that increase with temperature, reaching the maximum selectivity value of 14 % at the highest temperature tested.

The results of catalytic activity of V<sub>2</sub>O<sub>5</sub>-CeO<sub>2</sub> catalyst at T=250 °C as function of time are reported in Figure 4.

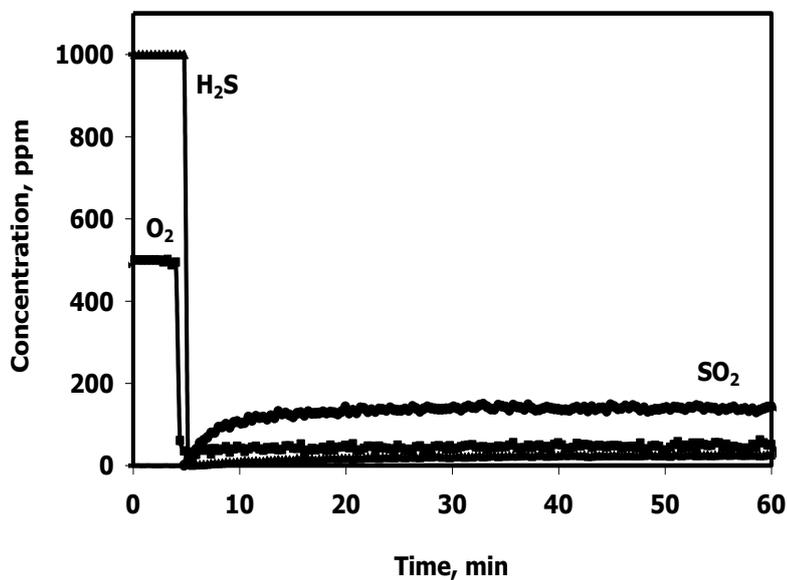


Figure 4: Stability test of V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> at T=250 °C (1000 ppm H<sub>2</sub>S, O<sub>2</sub>/H<sub>2</sub>S=0.5).

The figure shows that the catalyst in the first hour of time on stream any deactivation is evident, and the catalyst exhibits a very high H<sub>2</sub>S and O<sub>2</sub> conversion, but also a significant SO<sub>2</sub> concentration (140 ppm).

Further results concerning the effect of the gas hourly space velocity at constant inlet H<sub>2</sub>S concentrations and O<sub>2</sub>/H<sub>2</sub>S molar feed ratio on the SO<sub>2</sub> selectivity are showed in Table 1, where despite the sensible change in the GHSV values, any significant variations of the H<sub>2</sub>S, O<sub>2</sub> conversions and SO<sub>2</sub> selectivity are obtained.

Table 1: Effect of the gas hourly space velocity on the catalytic activity of V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> (T=250 °C, O<sub>2</sub>/H<sub>2</sub>S=0.5).

GHSV, h <sup>-1</sup>	X <sub>H<sub>2</sub>S</sub> , %	X <sub>O<sub>2</sub></sub> , %	Y <sub>SO<sub>2</sub></sub> , %
15,000	97	91	14
45,000	97	100	13

In Table 2 the effect of the inlet H<sub>2</sub>S concentration (from 250 ppm to 1000 ppm) in the feed gas at constant temperature and O<sub>2</sub>/H<sub>2</sub>S molar feed ratio are reported in terms of H<sub>2</sub>S conversion and SO<sub>2</sub> selectivity.

Table 2: Effect of the H<sub>2</sub>S concentrations on the catalytic activity of V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> (T=250 °C, O<sub>2</sub>/H<sub>2</sub>S=0.5).

H <sub>2</sub> S, ppm	O <sub>2</sub> , ppm	X <sub>H<sub>2</sub>S</sub> , %	Y <sub>SO<sub>2</sub></sub> , %
1000	500	98	14
500	250	98	17
250	125	100	26

In this case, the results reported in Table 2 show that there is a measurable effect of the initial concentration of H<sub>2</sub>S in the gas supply only on the selectivity to SO<sub>2</sub>.

Moreover, it is also evident that even significantly reducing the initial concentration of H<sub>2</sub>S, is not found a similar reduction in the selectivity to SO<sub>2</sub>.

In contrast with the very good results in terms of H<sub>2</sub>S conversion, the SO<sub>2</sub> selectivity is not so bad when the O<sub>2</sub>/H<sub>2</sub>S feed ratio is 0.5. As a consequence, additional catalytic tests were performed at lower O<sub>2</sub>/H<sub>2</sub>S molar feed ratio values, and the relevant results are reported in Table 3, where a very good result in terms of SO<sub>2</sub> selectivity was obtained for the O<sub>2</sub>/H<sub>2</sub>S value of 0.4, for which the SO<sub>2</sub> selectivity results drastically reduced from 13 % to 4 % without any significant reduction of the H<sub>2</sub>S and O<sub>2</sub> conversions.

Table 3: Effect of the feed ratio on the catalytic activity of V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> (T=250 °C, O<sub>2</sub>/H<sub>2</sub>S=0.5, GHSV=45,000 h<sup>-1</sup>)

O <sub>2</sub> /H <sub>2</sub> S	X <sub>H<sub>2</sub>S</sub> , %	X <sub>O<sub>2</sub></sub> , %	Y <sub>SO<sub>2</sub></sub> , %
0.5	97	100	13
0.4	94	100	4

#### 4. Conclusions

A vanadium-based catalyst supported on ceria with a nominal load of 2.55 %wt was prepared via impregnation method, and studied for the selective reaction of H<sub>2</sub>S oxidation to sulfur.

XRD and Raman characterization results showed that no signals relevant to the presence of isolated V<sub>2</sub>O<sub>5</sub>, suggesting that vanadium oxide is well dispersed on the CeO<sub>2</sub> surface.

The V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> catalyst showed very good performances in terms of catalytic activity, stability and SO<sub>2</sub> selectivity. The effect of the gas hourly space velocity and the inlet concentrations of H<sub>2</sub>S did not contribute to reduce significantly the SO<sub>2</sub> selectivity.

An interesting result to reduce SO<sub>2</sub> selectivity from 14 % to 4 %, was obtained by decreasing the O<sub>2</sub>/H<sub>2</sub>S feed ratio from the stoichiometric one (O<sub>2</sub>/H<sub>2</sub>S = 0.5) to a slightly lower value (O<sub>2</sub>/H<sub>2</sub>S = 0.4).

#### 5. Acknowledgments

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